

State Route 37 Sears Point to Mare Island Improvement Project Presenting to the San Francisco Bay Conservation Commission Engineering Criteria Review Board May 21, 2025

















Introductions

Caltrans:

- Javier Mendivil, PM
- Michael Bergman, Bridge Design
- Lewis Shen, Bridge Design
- Olivier Mbatchou, Roadway Design
- John Moore, Geotech
- Peter Wei, Geotech
- Jinpeng Li, Hydraulics
- Skylar Nguyen, Env Planning
- David Weber, Biology

Metropolitan Transportation Commission

- Kevin Chen Assistant Director
- Jeanette Weisman SR 37 Corridor Program Manager

AECOM Consultant Team

- Gary Sjelin, Hydraulics
- Brad Mays, Drainage
- Dillon Lennebacker, Environmental
- Joy Villafranca, Project Engineering Manager













Presentation Overview

- Project Overview
- Purpose and Need
- Proposed Elements in BCDC Jurisdiction
- General Overview
- Technical Discussion





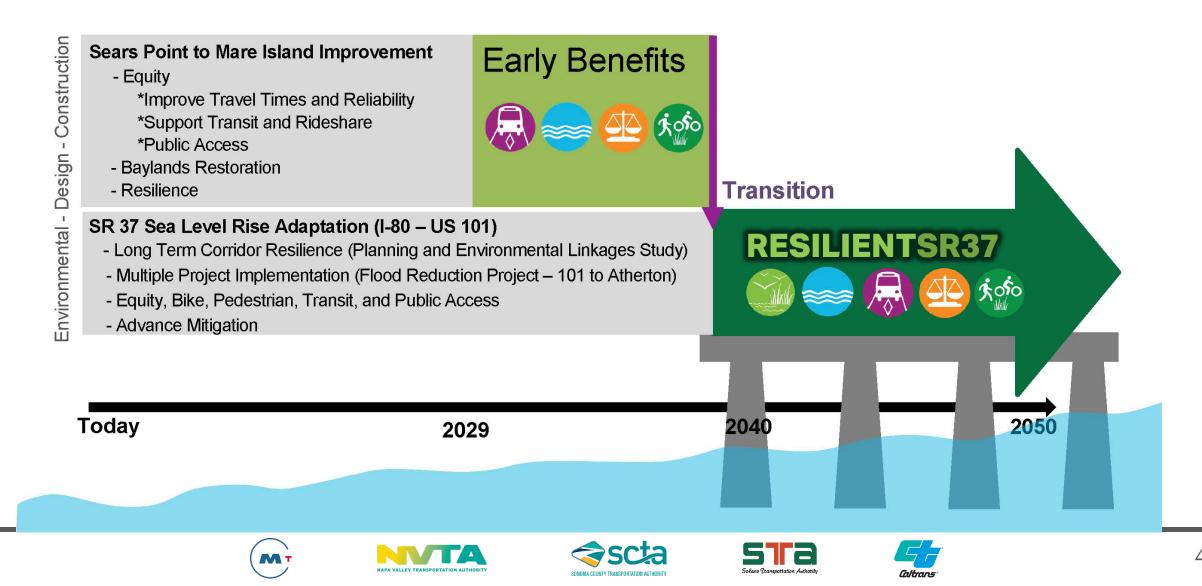








Phased Implementation





Project Location, Purpose, and Need

Location:

 Sonoma County SR 37 (PM 2.6 to 4.9) and SR 121 (PM 0 to 0.3)

Purpose:

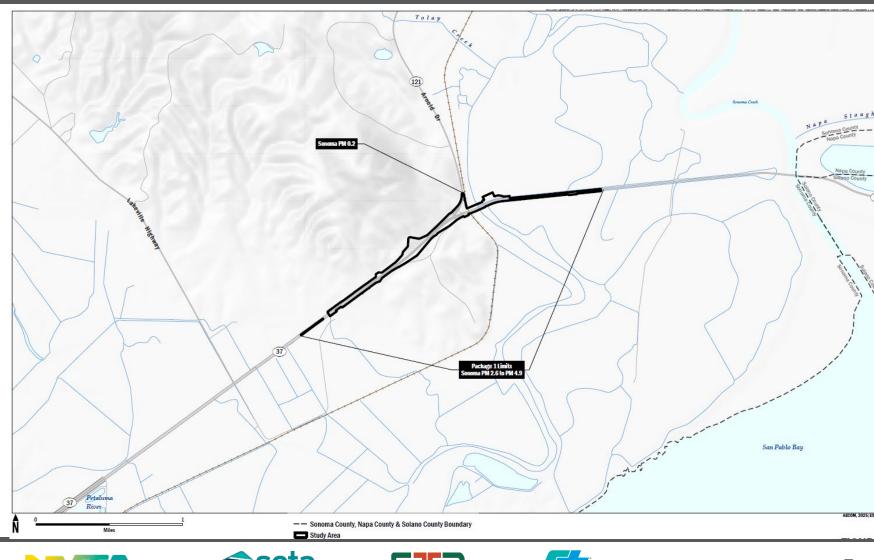
• Improve traffic flow

Need:

• Address recurring congestion

Minimization:

- Create waters/habitat
- Accommodate tidal prism









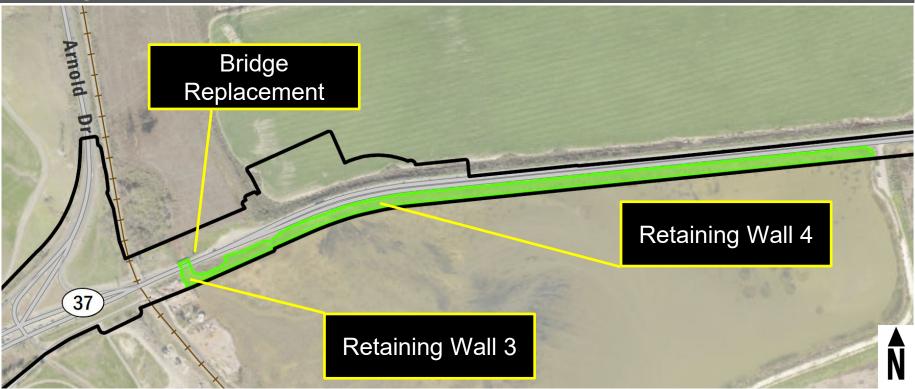




Project Components in BCDC

Project Elements

- Within BCDC Certain Waterway Jurisdiction
 - Tolay Creek Bridge Replacement
 - Retaining Walls 3 and 4
 - Fill Removal (creation of new waters from uplands)



Study Area

Potential BCDC Jurisdiction Feature

📃 Certain Waterway









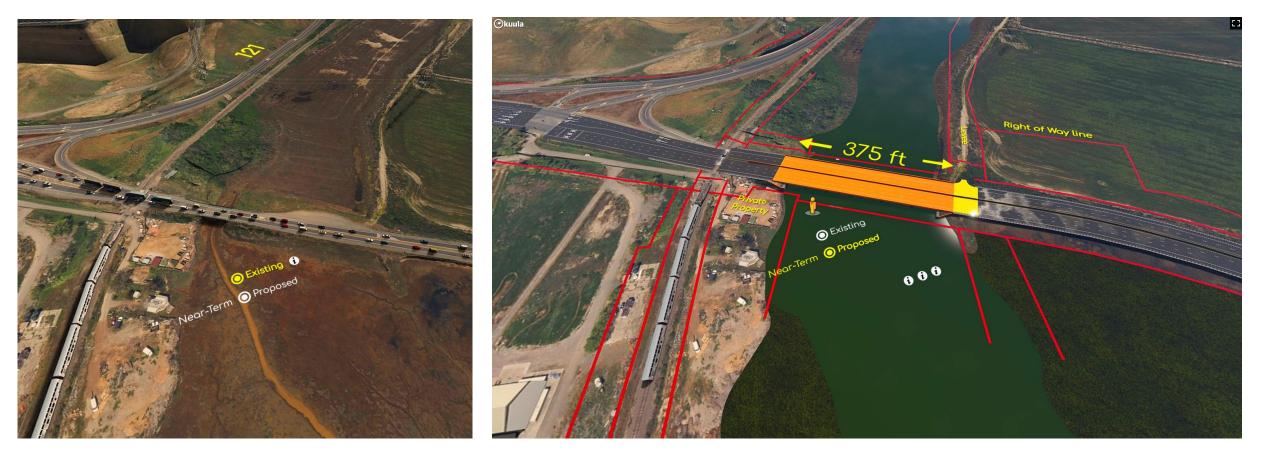




Tolay Creek Bridge Replacement

Existing

New Bridge









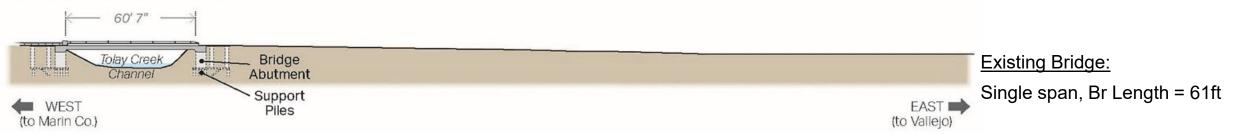




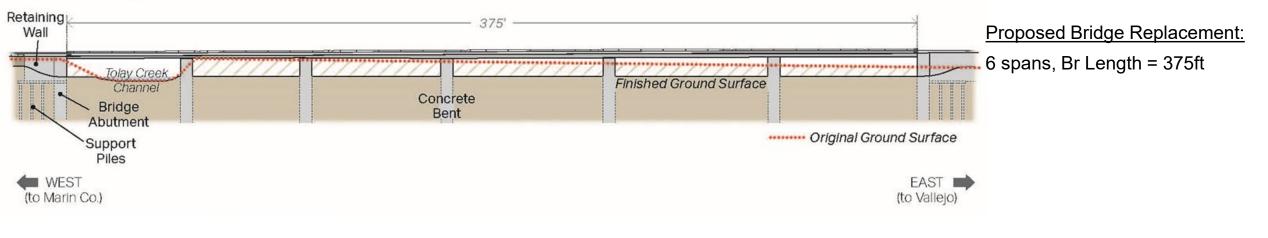


Tolay Creek Bridge - Replacement Configuration





Proposed Bridge







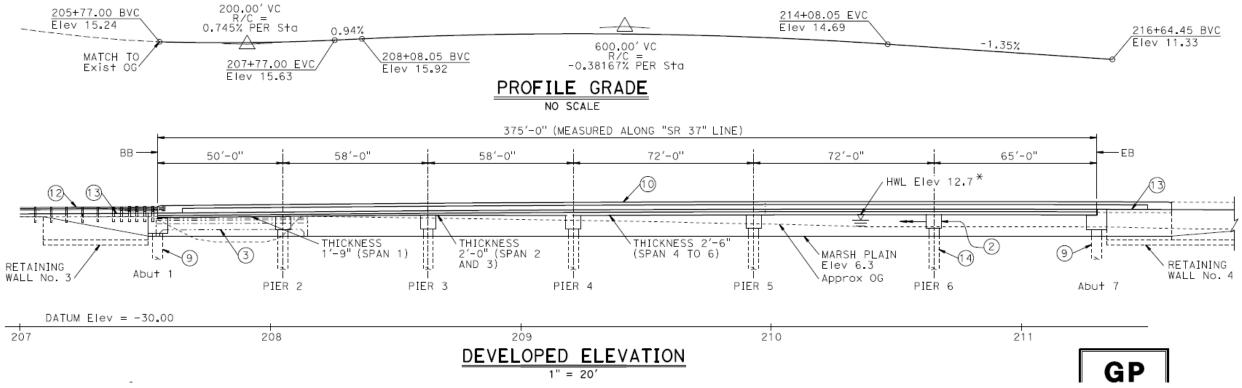








Tolay Creek Bridge – Span Configuration



- Precast/prestressed voided slab w/ CIP deck continuous superstructure.
- Drop Bentcap on Pile Extensions. Additional bentcap width added to support the superstructure during fault rupture.





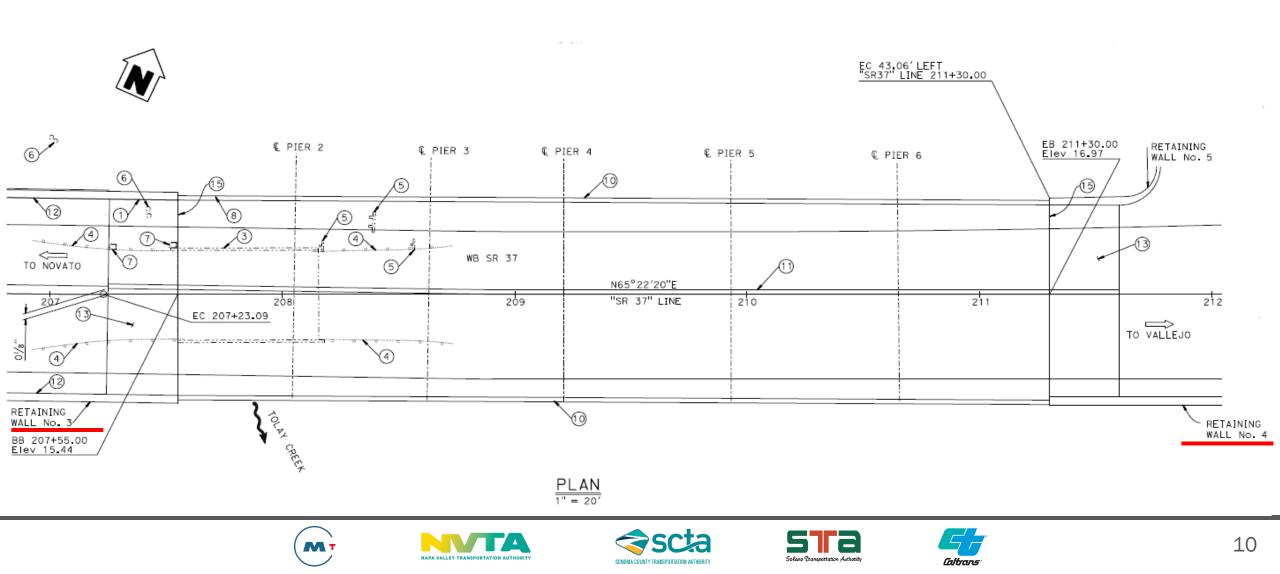






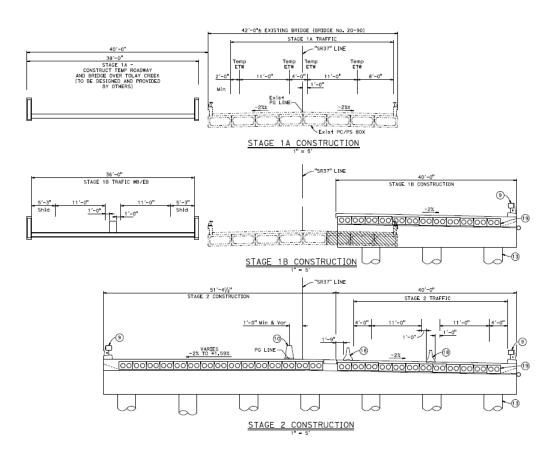


Tolay Creek Bridge – Plan View





Tolay Creek Br – Typical Section/Stage Construction



Stage 1 Construction:

- Temp Traffic Detour with Temp Bridge
 over exist Tolay Crk
- Constructing partial new Tolay Crk Br to the South.

Stage 2 Construction:

- Traffic on newly constructed partial Tolay Crk Br to the south.
- Construct partial Tolay Crk Br to the North.







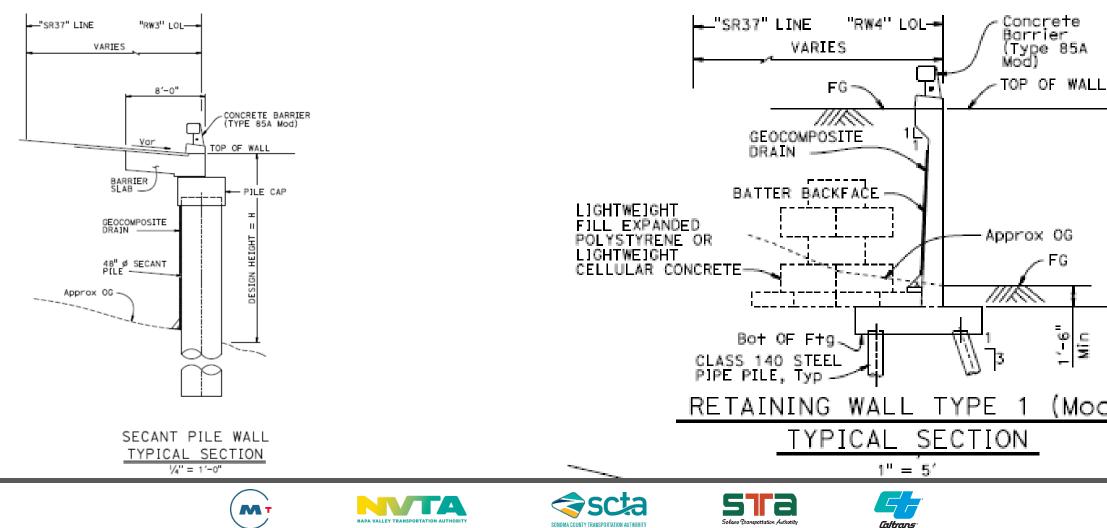






Retaining Walls – Typical Section

Retaining Wall 3



Retaining Wall 4, 5

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DESIGN HEIGHT

FG

-6" Min

(Mod)

-



DESIGN GENERAL NOTES

TOLAY CREEK BRIDGE

<u>Design</u>

- AASHTO LRFD Bridge Design Specs 2017, with CA Amendments updated June 2024
- Standard Plans and Specs, 2024 with Revised Standard Plans April 2025
- Seismic Design
- Caltrans Seismic Design Criteria, Version 2.0, April 2019
- Fault Rupture: (Static Offset)
- Horizontal Design Offset = 1.7 feet
- Vertical Design Offset = 0.9 feet
- Dead Load
- Includes 1" Polyester overlay
- Live Loading
- HL93 and permit design load

RETAINING WALLS 3, 4 & 5

<u>Design</u>

- AASHTO LRFD Bridge Design Specs 2017, with CA Amendments updated June 2024
- Standard Plans and Specs, 2024 with Revised Standard Plans April 2025

Soil Parameters (Lightweight EPS block)

- Φ = 27°
- γ = 35 pcf
- Kn = 0.35
- Kv = 0
- Kα = 0.38









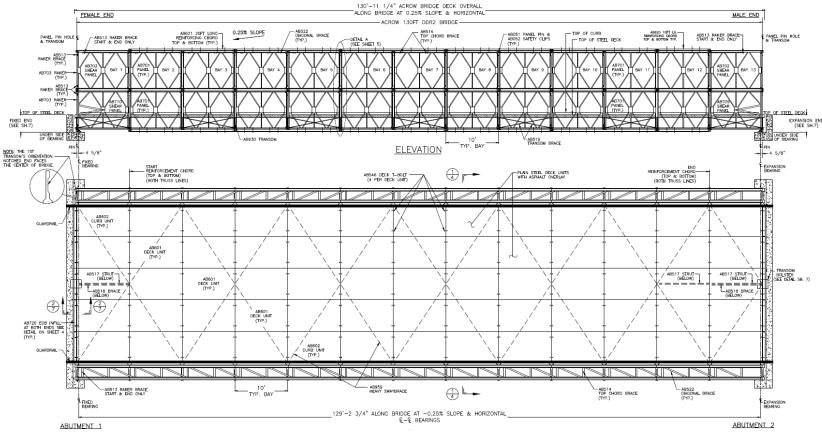




TEMPORARY BRIDGE STRUCTURE



Example of one type, Acrow Br Co. Temporary bridge type will be selected by the Construction Contractor

















Tolay Creek Bridge – Geotechnical Investigation















Field investigation from 2023 to 2025

- Four mud rotary wash soil borings up to 161.5 feet in depth
- Field testing included standard penetration testing (SPT) and pocket penetration testing (PP) during drilling
- Eight cone penetration testing (CPT) up to 119 feet in depth
- Three seismic measurements during CPT pushing
- A review of five As-built log of test borings (LOTB) drilled in 1973



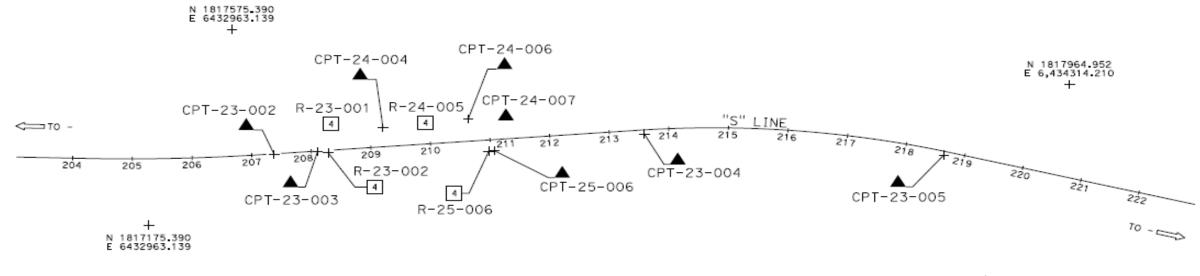












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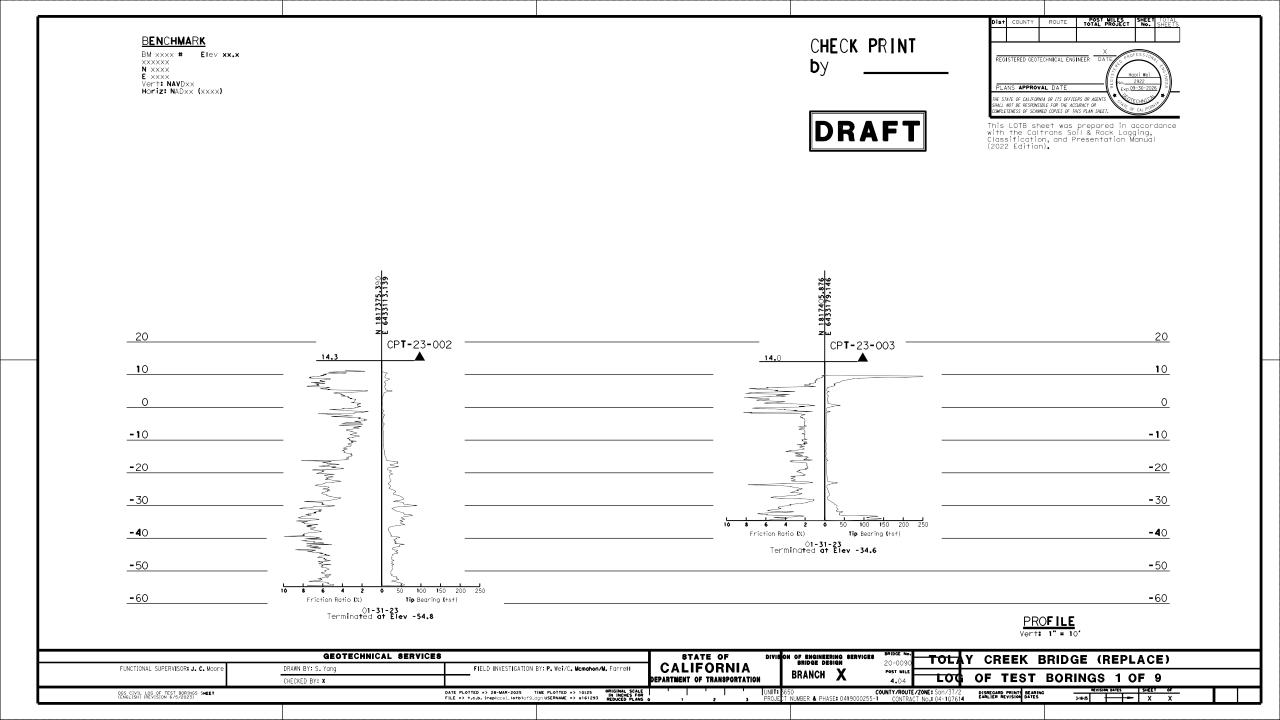






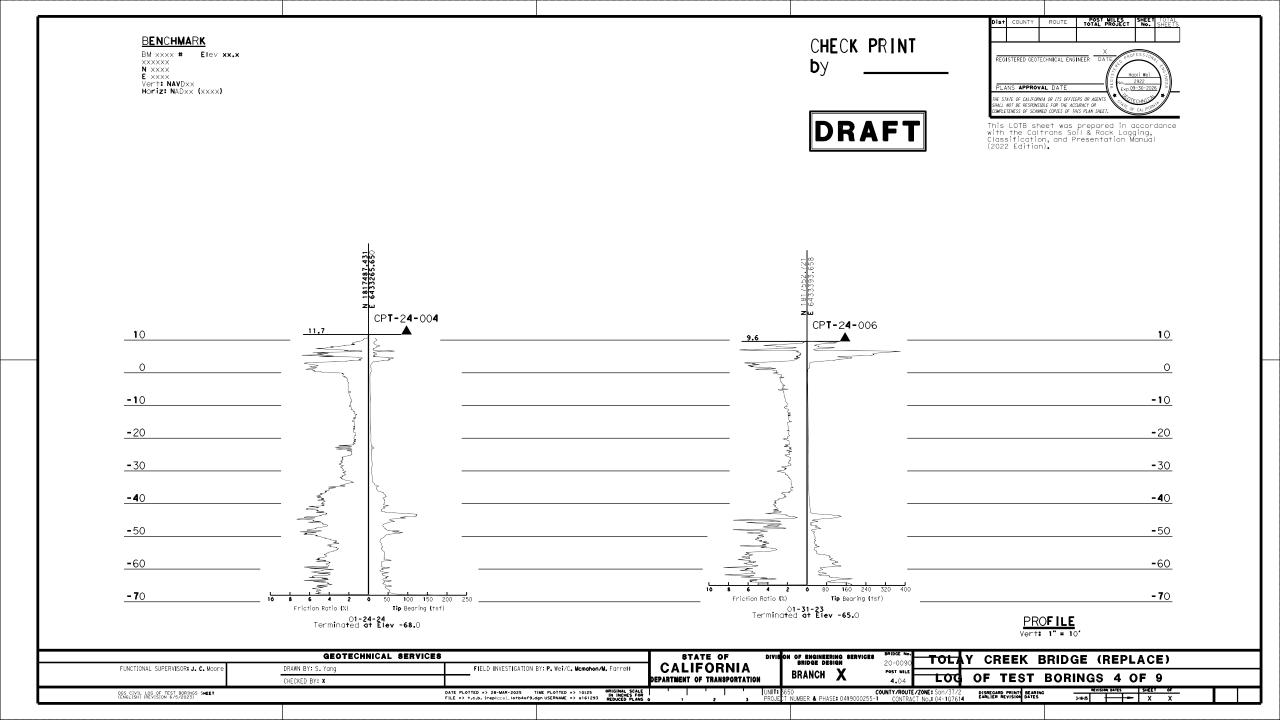






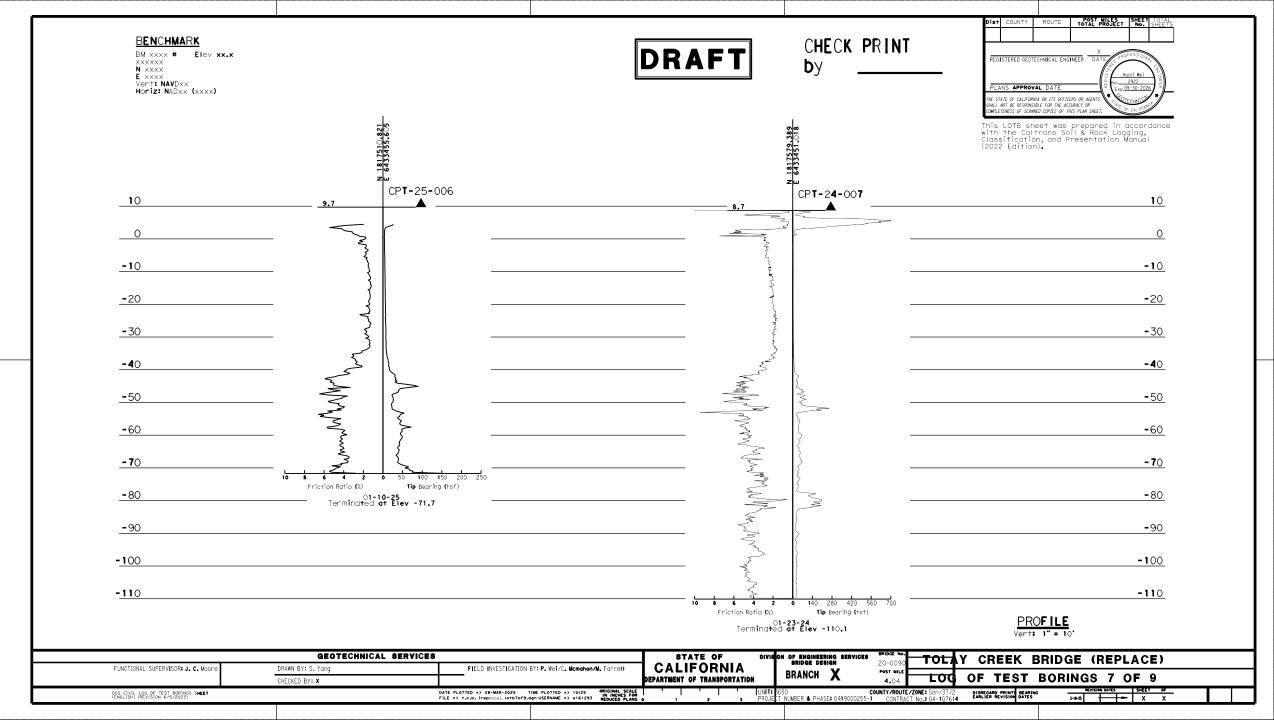
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-40	Poorly-graded GRAVEL wi	ith CLAY and SAND (GP-GC); medium dense; brown; we	t; fine to coarse GRAVEL; medium to coarse SAND.	-40
			ine to coarse SAND; low plasticity fines; PP=2.0 tsf.	
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	-PP>4.5 tsf.			
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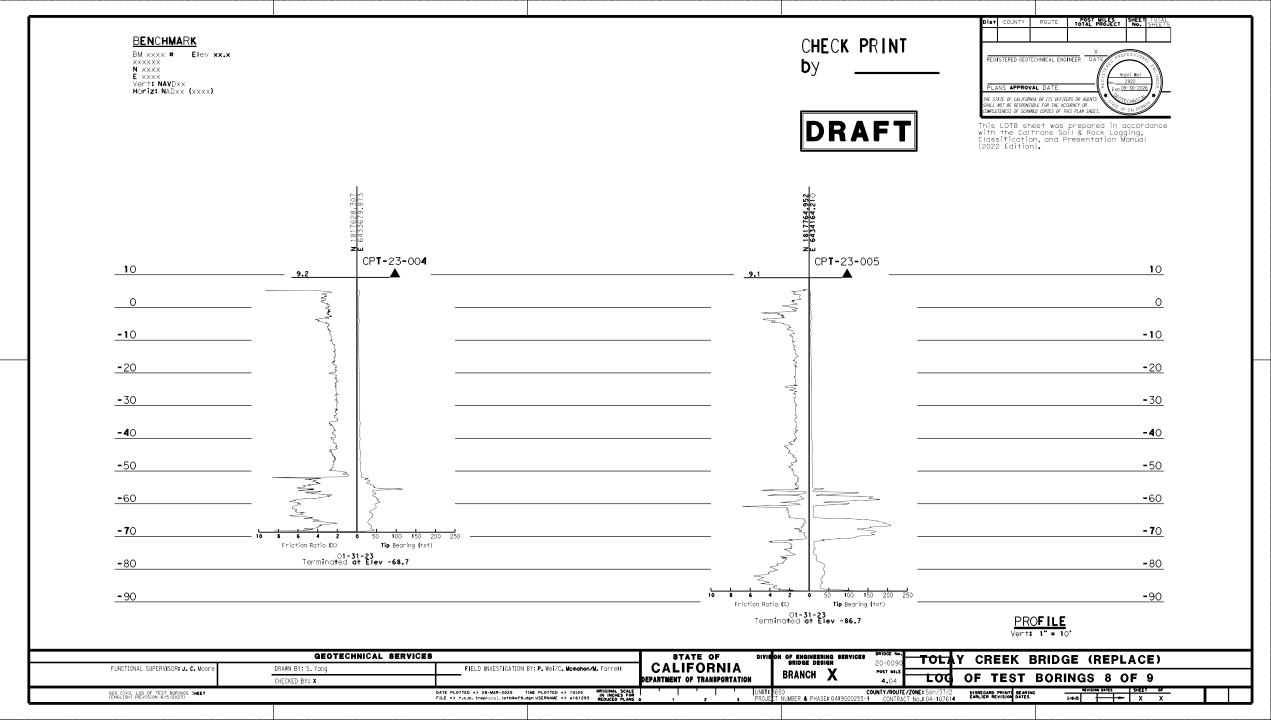
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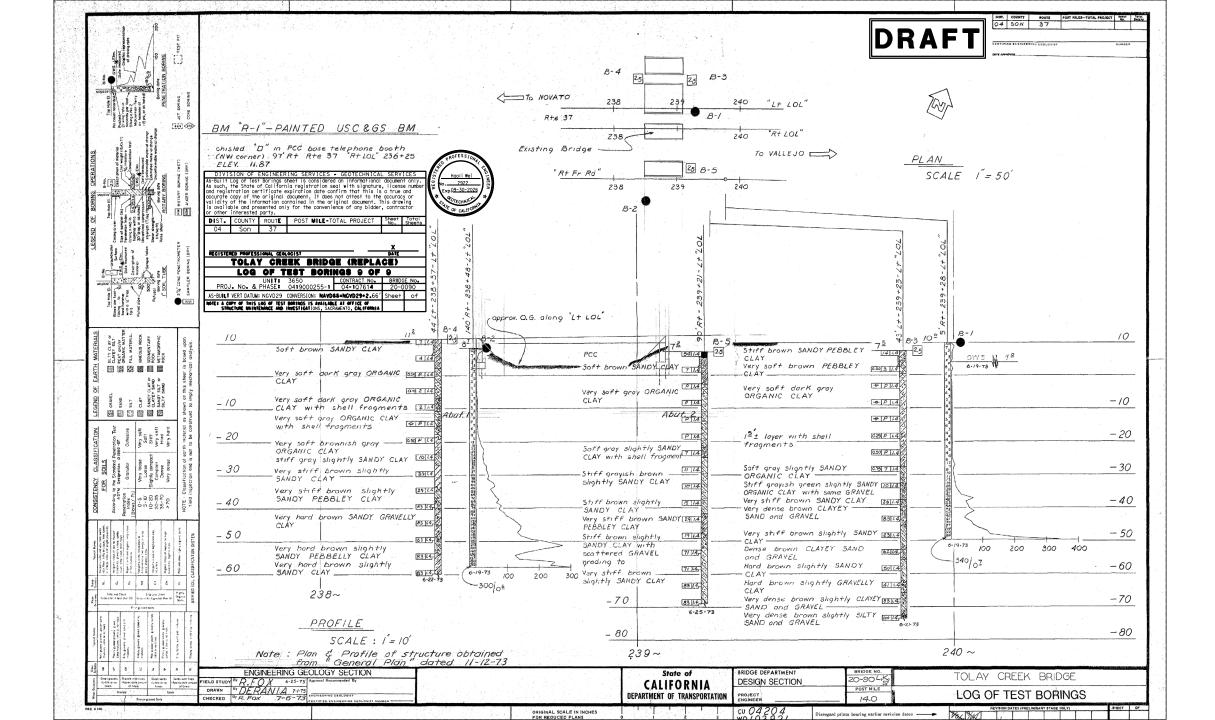


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- <u>120</u> - <u>130</u>	Lean CLAY with SAND (CL); very stiff; yellowish brown; wet; fine to coarse SAND; high plasticity fines; PP=2.5 tsf
-140	-140
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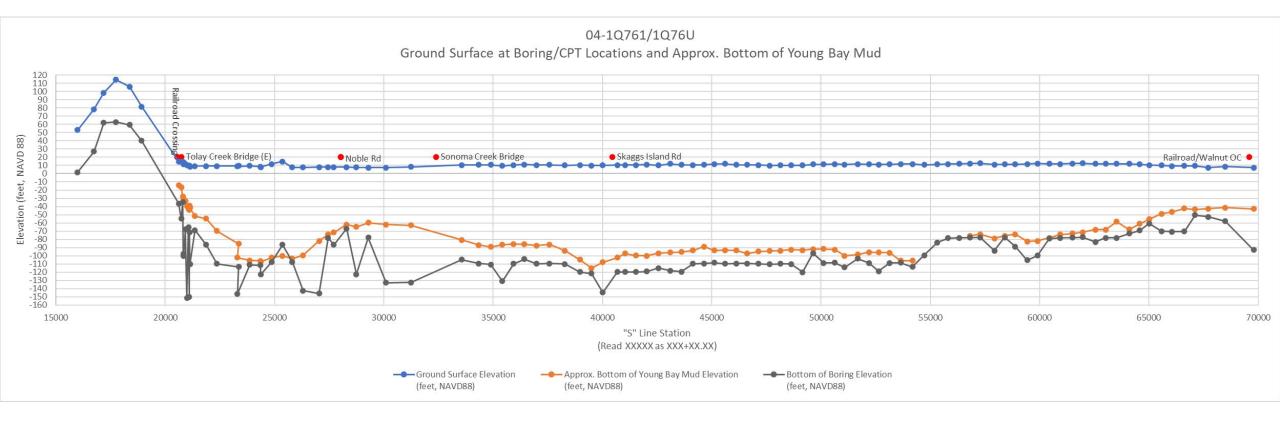
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·50	Lean CLAY with SAND (CL); very stiff; light brown with gray; wet; trace fine, subangular to subrounded GRAVEL; medium SAND; high plasticity fines; PP=3.0 tsf.	50
	1711-4 -PP=3.75 tsf. 12511-4 -hard; PP>4.5 tsf.	
60		·60
-	-hard; trace pebbles and gravels; PP>4.5 tsf.	-
70	SANDY fat CLAY (CH); stiff; light grayish brown; wet; high plasticity fines; sample left in hole overnight; PP=1.5 tsf.	7 0
.80	Lean CLAY with GRAVEL (CL); hard; pale brown; wet; angular GRAVEL; little medium SAND; high plasticity fines; PP>4.5 tsf.	80
	ESTIM Lean CLAY with SAND (CL); hard; light brown; wet; angular to subangular GRAVEL; coarse to fine SAND; high plasticity fines; PP>4.5 tsf.	<u></u>
•90	Image: Second CLAY (CL); hard; light to olive brown; wet; trace fine SAND; high plasticity fines; some calcium carbonate nodules; PP>4.5 tsf. Image: Second calcium carbonate calcium carbonate nodules; PP>4.5 tsf.	90
	-light grayish brown; few fine GRAVEL; PP>4.5 tsf.	
100	-1 SANDY lean CLAY with GRAVEL (CL); hard; pale yellowish brown; wet; subangular to subrounded GRAVEL; medium to fine SAND; medium to high plasticity fines;	00
10	PP>4.5 tsf. -few GRAVEL ; few medium to fine SAND; PP=4.25 tsf.	10
10		10
20	-some calcium carbonate nodules; PP>4.5 tsf.	20
	I23II.4 -very stiff; sample left in hole overnight; PP=3.0 tsf. I36II.4 -hard; little medium to fine SAND; PP>4.5 tsf.	
130		30
40	-trace SAND; some calcium carbonate nodules; PP=4.25 tsf.	
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150	CLAYEY SAND with GRAVEL (SC); very dense; light brown; wet; fine GRAVEL; coarse to fine SAND. Lean CLAY (CL); very stiff; light brown; wet; trace fine SAND; medium plasticity fines; PP=3.25 tsf.	50
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Laboratory Testing included:

- Moisture content
- Particle gradation
- Atterberg limits
- Unconfined compression
- Consolidation
- Consolidated undrained triaxial
- Corrosion













Subsurface conditions

- Fill thickness including AC/AB sections from 3 to 10 feet
- Very soft to soft clayey soils (young bay mud) from 34 to 60 feet in thickness
- Young bay mud thickness increases from west to east
- Stiff to hard clayey soils with a few layers of medium dense to very dense sand (consolidated bay mud) below young bay mud up to maximum depths drilled





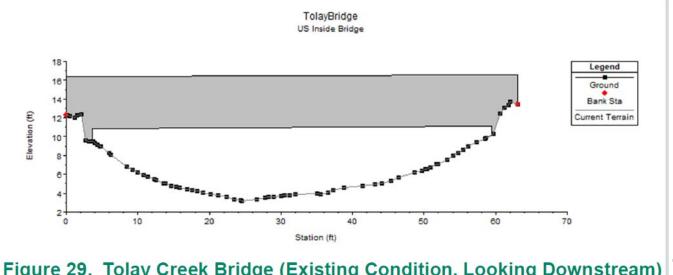




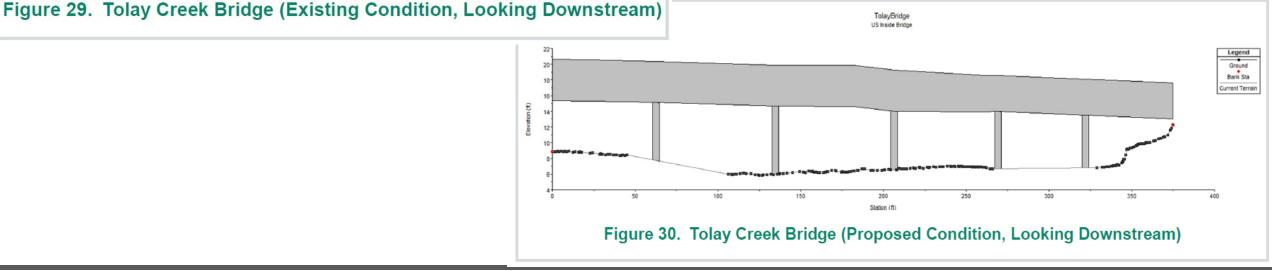




Tolay Creek Bridge – Hydraulics



- Hydraulic study and report were prepared for the bridge
- HEC-RAS was used to develop a 2D model of the bridge
- HEC-RAS 2D hydrodynamic model was run for 12 scenarios developed from criteria in the Caltrans Highway Design Manual













Sea Level Rise Considerations

TABLE 6. Sea Level Scenarios for San Francisco.

Current OPC Guidance (2024)

- 0.8 to 1.3 Feet of SLR by 2050 Project Assumptions
- 9.9 feet 100-year maximum water surface elevation
- 1 foot wave crest
- 0.7 Feet of SLR by 2046
- 1 foot of freeboard
- Minimum Soffit elevation 12.6 feet

Median values of Sea Level Scenarios, in feet, for each decade from 2020 to 2150, with a baseline of 2000. All median scenario values incorporate the local estimate of vertical land motion.

YEAR	LOW	INT-LOW	INTERMEDIATE	INT-HIGH	нібн
2020	0.2	0.2	0.2	0.3	0.3
2030	0.3	0.4	0.4	0.4	0.4
2040	0.4	0.5	0.6	0.7	0.8
2050	0.5	0.6	0.8	1.0	1.3
2060	0.6	0.8	1.1	1.5	2.0
2070	0.7	1.0	1.4	2.2	2.9
2080	0.8	1.2	1.8	3.0	4.1
2090	0.9	1.4	2.4	3.8	5.3
2100	1.0	1.6	3.1	4.8	6.5
2110	1.0	1.8	3.8	5.6	7.8
2120	1.1	2.0	4.4	6.4	9.0
2130	1.2	2.2	4.9	7.0	9.9
2140	1.3	2.4	5.4	7.6	10.8
2150	1.3	2.6	6.0	8.1	11.7













Tolay Creek Bridge – Design Criteria/Model Assumptions

Table 7. Future Condition Model Scenarios

Scenario	Event Frequency	Precipitation Frequency	Tide at Peak Flow
9	100-Year	100-Year	MSL (3.70 Ft + 2.00 Ft Surge + 0.70 Ft SLR)
10	100-Year	50-Year	MHHW (6.42 Ft + 2.00 Ft Surge + 0.70 Ft SLR)
11	100-Year	No Precipitation	EHW (7.12 Ft + 2.00 Ft Surge + 0.70 Ft SLR)
12	50-Year	50-Year	MSL (3.70 Ft + 2.00 Ft Surge + 0.70 Ft SLR)

- The table outlines the most conservative modeling scenarios for the SR-37 Tolay Creek Bridge, incorporating a
 planning horizon of 2046 with a sea level rise (SLR) of 0.7 feet based on the 2024 California guidance.
- Scenarios include a range of precipitation frequencies combined with tidal conditions adjusted for surge and SLR.
- Tidal levels at peak flow are set at Mean Sea Level (MSL), Mean Higher High Water (MHHW), and Extreme High Water (EHW), each with a 2-foot surge and 0.7-foot SLR added.
- These assumptions reflect a conservative approach to account for future climate impacts and tidal influences on the hydraulic design of the proposed bridge.





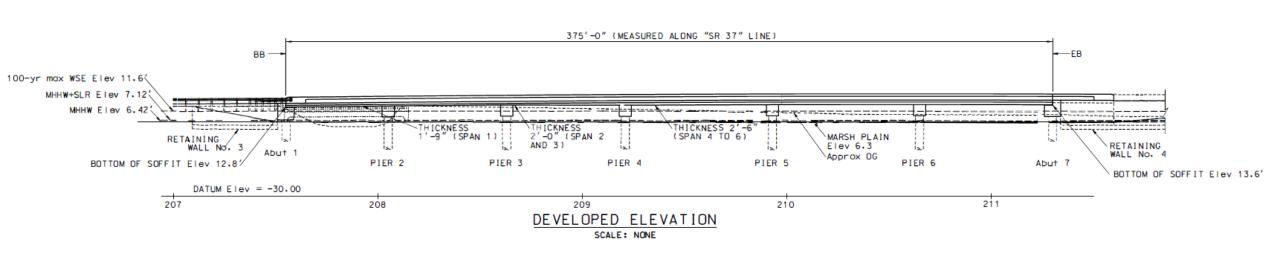








SLR Considerations







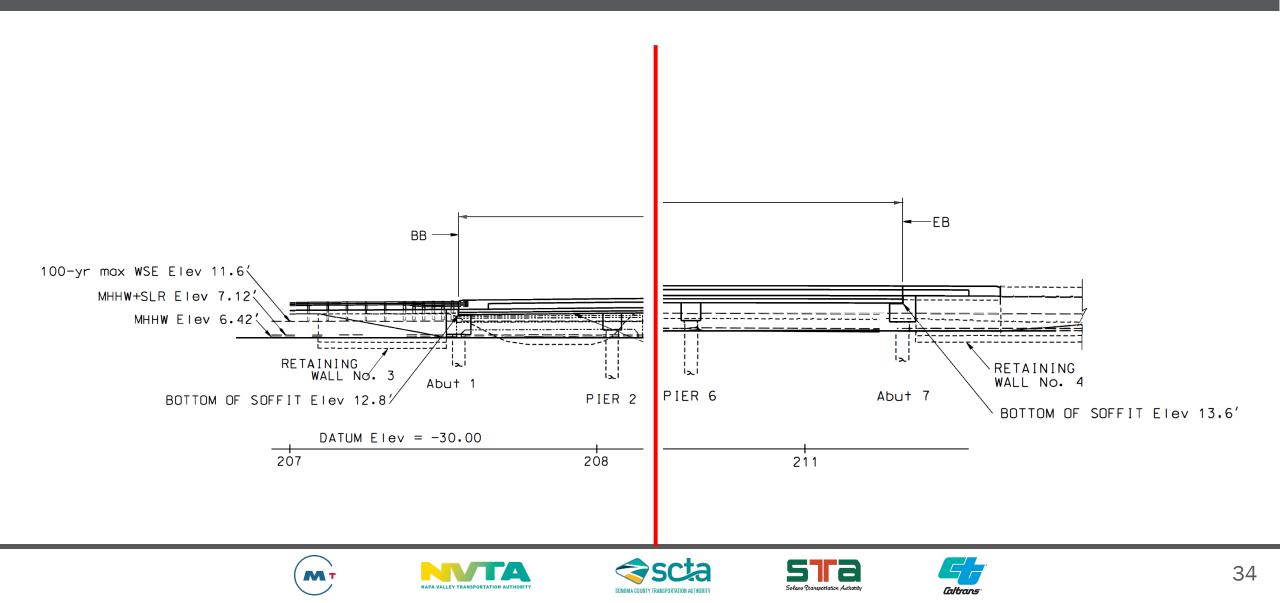
















Part 3 - Issues and Applications in Coastal Highway Design

HEC-25 3rd ed.

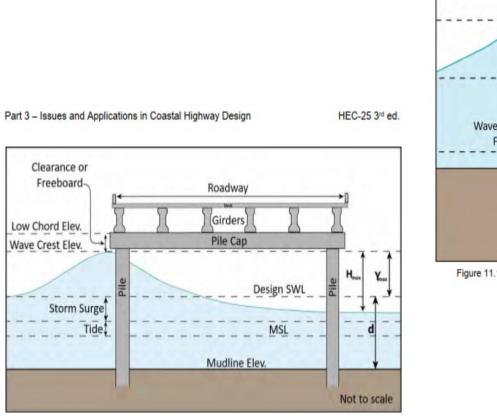
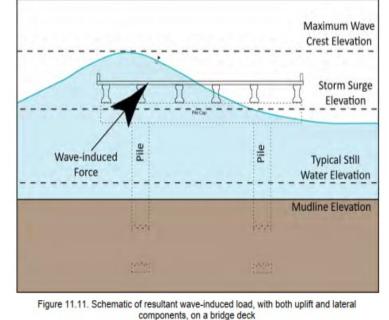


Figure 11.16. Definition sketch of wave parameters and water levels for determining elevation of bridge deck for clearance from wave crests



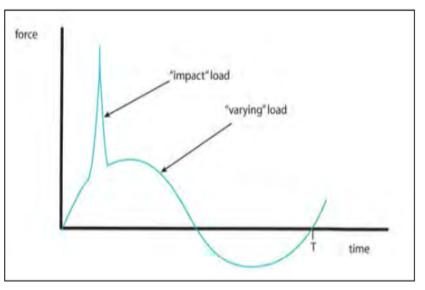


Figure 11.12. Schematic of typical time-history of wave loads on rigid structures















Scenario	Event Frequency (Years)	East Branch Maximum Discharge (cfs)	Tolay Bridge Maximum Discharge (cfs)	Maximum Water Surface (feet, NAVD 88)	Maximum Velocity (feet per second)
9	100	-19/+371	-136/+530	+8.95	1.2
10	100	-6/+289	-140/+408	+8.97	1.0
11	100	-21/+28	-332/+49	+9.45	0.7
12	50	-19/+286	-135/+422	+8.73	1.1

Table 10. Future Condition Scenario Results

- The most conservative result is from Scenario 11, occurring during an extreme high water tide cycle.
- Maximum discharge through the Tolay Creek Bridge -332 cfs (upstream) and +49 cfs (downstream) in Scenario 11, reflecting significant tidal influence.
- The maximum velocity of 1.2 feet per second is observed in Scenario 9, aligning with a 100-year precipitation event and MSL tide conditions with surge and SLR.
- These results suggest lower flow rates and velocities compared to previous studies, attributed to reduced SLR assumptions (0.7 ft vs. 1.7 ft) and storage effects in the upstream marsh.
- The recommended minimum soffit elevation of +12.60 feet (NAVD 88) accounts for the +9.90 ft EHW, 1 ft wave crest, 0.7 ft SLR, and 1 ft freeboard, ensuring safety against future conditions.













Thank you!













